

Current Driver for Infrared LED

Week 6: Digital-to-Analog Conversion

ECE 327: *Electronic Devices and Circuits Laboratory I*

Abstract

In the digital-to-analog conversion (DAC) lab, the output of the JK flip-flop used in the analog-to-digital conversion (ADC) lab needs to drive a heavy load. The flip-flop output can only supply 1 mA maximum, but the infrared LED needs to be driven by at least 10 mA and probably will need to operate at 35–50 mA in this lab. So we need to build a current driver. Current drivers can easily be built with a single NPN or PNP transistor acting as either a current source or sink. Here, we review the prototypical follower and switch circuits that could be used as drivers in this laboratory.

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1 LED Operation

The QEE113 infrared light-emitting diode (LED) should be operated with a current limiting resistor, as shown in Figure 1.1, so that the forward current through the diode is between 10 mA and 50 mA.

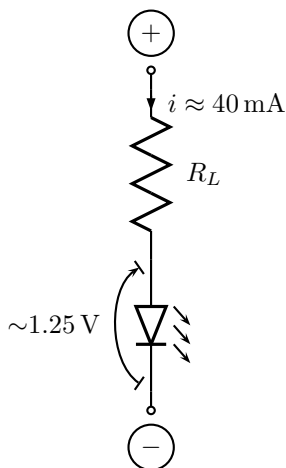


Figure 1.1: Typical operation of QEE113 infrared light-emitting diode (LED).

In this laboratory, a forward current of 40 mA (or less) will be sufficient for eye-to-eye transmission of up to $\sim 0.5 \text{ m}$ to a QSE157 receiver. At 40 mA, the potential drop across the LED is 1.25–1.30 V. We use this approximation to derive a nominal value for current-limiting resistor R_L .

In the following, we show four different current driver architectures. In section 2, we show an NPN transistor being used as a current *source* in a follower (i.e., active) configuration and as a current *sink* in a switch (i.e., saturation) configuration. In section 3, we show a PNP transistor being used as a current *source* in a switch (i.e., saturation) configuration and as a current *sink* in a follower (i.e., active) configuration.

2 NPN Current Drivers

In both driver configurations shown in Figure 2.1, the current-limiting resistance R_L must be set to deliver $i \approx 40$ mA to the LED.¹

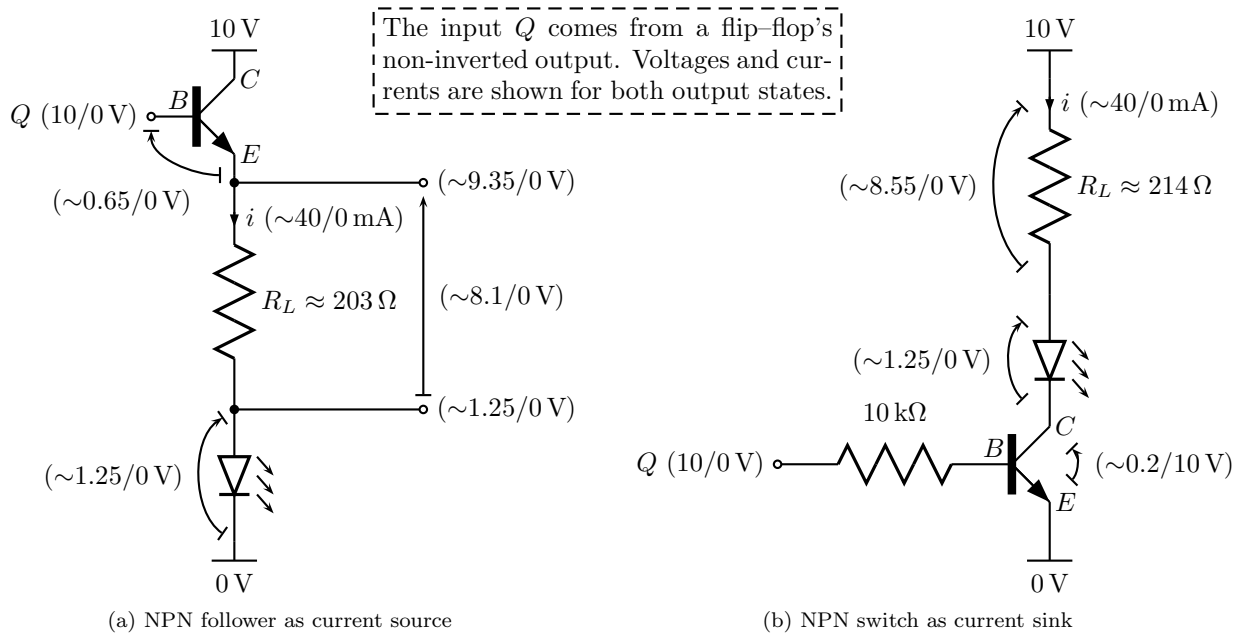


Figure 2.1: NPN (2N3904) current drivers for QEE113 infrared LED. The follower configuration in (a) biases the transistor into *active* mode. The switch configuration in (b) biases the transistor into *saturation* mode. Circuit values are shown for both *high* and *low* logic input Q . In the *low* case, transistor current is *cutoff*.

Although R_L can be implemented with a variable resistor (e.g., two adjacent pins of a potentiometer), tuning its value² may have less of an impact than tuning the distance between the QEE113 and the QSE157.

NPN Current Source

In Figure 2.1(a), with input Q *high*, the transistor is in *active* mode. A BJT transistor in this mode *dynamically adjusts* its effective collector-emitter resistance so that the base-emitter potential is maintained at approximately 0.65 V. Therefore, the resistor–diode combination is driven by 0 V or 9.35 V depending on whether Q is *low* or *high*, respectively. To make the high current equal to 40 mA, the current-limiting resistor

$$R_L \approx \frac{8.1 \text{ V}}{40 \text{ mA}} = 202.5 \Omega. \quad (2.1)$$

NPN Current Sink

In Figure 2.1(b), with input Q *high*, the transistor is in *saturation* mode. A BJT transistor in this mode is not able to reduce its collector-emitter potential any farther. So it assumes a value of approximately 0.2 V. Therefore, the resistor–diode combination is driven by 0 V or 9.8 V depending on whether Q is *low* or *high*, respectively. To make the high current equal to 40 mA, the current-limiting resistor

$$R_L \approx \frac{8.55 \text{ V}}{40 \text{ mA}} = 213.75 \Omega. \quad (2.2)$$

¹Active-mode analysis uses rail-to-rail logic assumption that is untrue for TTL; however, BJT saturation mode is slow.

²That is, **increase current** if too little power is received and **decrease current** if the receiver triggers too easily.

3 PNP Current Drivers

In both driver configurations shown in Figure 3.1, the current-limiting resistance R_L must be set to deliver $i \approx 40$ mA to the LED.³ **NOTE THAT \bar{Q} , NOT Q , is used as an input.**

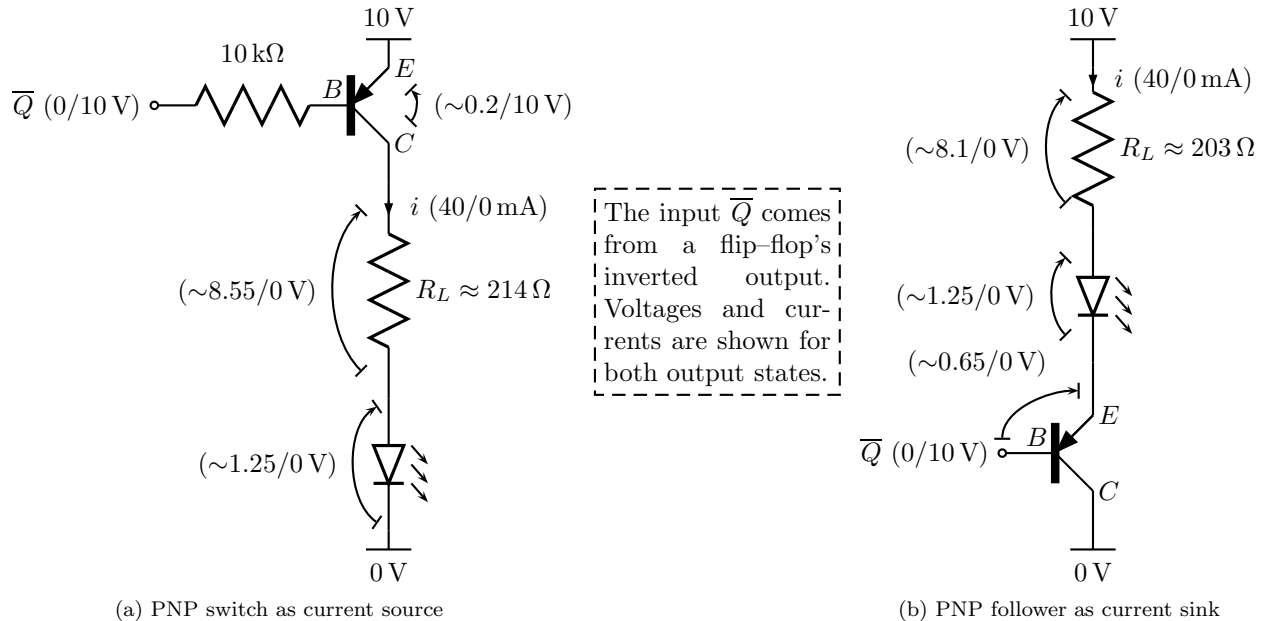


Figure 3.1: PNP (2N3906) current drivers for QEE113 infrared LED. The switch configuration in (a) biases the transistor into *saturation* mode. The follower configuration in (b) biases the transistor into *active* mode. Circuit values are shown for both *low* and *high* input \bar{Q} . In the *high* case, transistor current is *cuttoff*.

Although R_L can be implemented with a variable resistor (e.g., two adjacent pins of a potentiometer), tuning its value⁴ may have less of an impact than tuning the distance between the QEE113 and the QSE157.

PNP Current Source

In Figure 3.1(b), with input Q *high*, the transistor is in *saturation* mode. A BJT transistor in this mode is not able to reduce its collector-emitter potential any farther. So it assumes a value of approximately 0.2 V. Therefore, the resistor–diode combination is driven by 0 V or 9.8 V depending on whether Q is *low* or *high*, respectively. To make the high current equal to 40 mA, the resistor current-limiting resistor nominally be

$$R_L \approx \frac{8.55 \text{ V}}{40 \text{ mA}} = 213.75 \Omega. \quad (3.1)$$

PNP Current Sink

In Figure 3.1(a), with input Q *high*, the transistor is in *active* mode. A BJT transistor in this mode *dynamically adjusts* its effective collector-emitter resistance so that the base-emitter potential is maintained at approximately 0.65 V. Therefore, the resistor–diode combination is driven by 0 V or 9.35 V depending on whether Q is *low* or *high*, respectively. To make the high current equal to 40 mA, the resistor current-limiting resistor nominally be

$$R_L \approx \frac{8.1 \text{ V}}{40 \text{ mA}} = 202.5 \Omega. \quad (3.2)$$

³Active-mode analysis uses rail-to-rail logic assumption that is untrue for TTL; however, BJT saturation mode is slow.

⁴That is, **increase current** if too little power is received and **decrease current** if the receiver triggers too easily.

A Parts

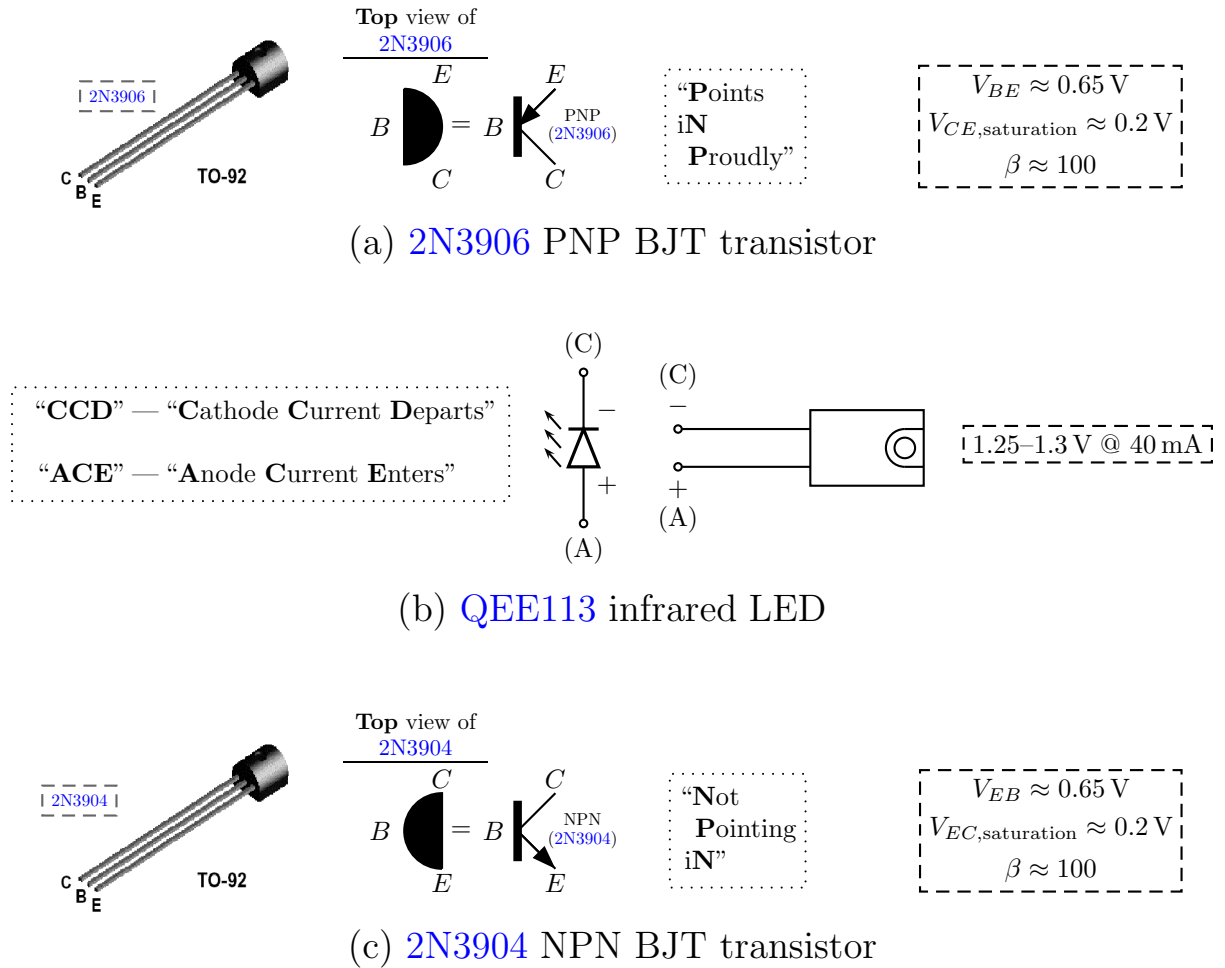


Figure A.1: Part pin-outs.